

EFFECTS OF WATERSHED RESTORATION ON HILLSLOPE STABILITY AND ECOHYDROLOGICAL FUNCTIONS

Mapping Project Report

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1. LiDAR System Description and Specifications

This survey was performed with an Optech GEMINI Airborne Laser Terrain Mapper (ALTM) serial number 06SEN195 mounted in a twin-engine Cessna Skymaster (Tail Number N337P). The instrument specifications are listed in table 1.

Operating Altitude	150 - 4000 m, Nominal
Horizontal Accuracy	1/5,500 x altitude (m AGL); 1 sigma
Elevation Accuracy	5 - 30 cm; 1 sigma
Range Capture	Up to 4 range measurements, including 1 st , 2 nd , 3 rd , last returns
Intensity Capture	12-bit dynamic range for all recorded returns, including last returns
Scan FOV	0 - 50 degrees; Programmable in increments of ±1degree
Scan Frequency	0 – 70 Hz
Scanner Product	Up to Scan angle x Scan frequency = 1000
Roll Compensation	±5 degrees at full FOV – more under reduced FOV
Pulse Rate Frequency	33 - 167 kHz
Position Orientation System	Applanix POS/AV 510 OEM includes embedded BD950 12-

	channel 10Hz GPS receiver
Laser Wavelength/Class	1047 nanometers / Class IV (FDA 21 CFR)
Beam Divergence nominal (full angle)	Dual Divergence 0.25 mrad (1/e) or 0.80 mrad (1/e)

Table 1 – Optech GEMINI specifications.

See <u>http://www.optech.ca</u> for more information from the manufacturer. <u>http://www.optech.ca/pdf/Brochures/ALTM-GEMINI.pdf</u>

2. Description of PI's Areas of Interest.

The areas of interest are two experimental watersheds, Shotgun Creek and Twin Creek located in the Clearwater National Forest of northern Idaho. These areas are roughly 70 km southwest of Missoula, MT. and are delimited by two irregular polygons as shown in figure 1 (Google Maps image). The survey polygon for Shotgun Creek (Area 1) is approximately 15.8 square kilometers and for Twin Creek (Area 2) is 26.34 square kilometers. The polygon for area 1 is roughly 5 km long in the East-West orientation and 3.5 km long in the North-South direction. Area 2 has a maximum length of 8.86 km in the 155°azimuth with an average width of 2.77 km.



Figure 1 – Shape and location of survey polygon (Google Maps).

3. Airborne Survey Planning Process.

The survey planning was performed considering nominal values of 650m for flight altitude above the terrain, a mean flying speed of 60 m/s and a swath overlap of 50%. Taken into account these values and the layout of the areas of interest the optimized flight plan consisted of a total of 45 flight lines, 19 for Shotgun creek at azimuths of 90/270° and 26 for Twin creek at azimuths of 155/335°. In order to obtain the highest point density the laser Pulse Repetition Frequency (PRF) was set to 70 kHz. Scan frequency (mirror oscillation rate) was held to 40 Hz and the scan angle (Field-of-View or FOV) was limited to +/- 21 degrees. These parameters yield a scan product (frequency x angle) of 840 out of a system maximum of 1000, or about 84% of system limits. The combination of all these parameters should yield a point density of 4.7 points per m². Figure 2 show screen captures from the planning software displaying the planned flight lines along with other survey parameters for the Shotgun Creek area; these are also summarized in table 2.



Figure 2. East-West flight lines for Shotgun Creek from the planning software.

Nominal Flight	Parameters	Equipment S	ettings	Area Totals	
Flight Altitude	650 m	Laser PRF	70 kHz	Total Passes	19
Flight Speed 60 m/s Beam Diverger		Beam Divergence	0.25 mrad	Total Length	89.749 km
Swath Width 422.4 m Scan Frequency		40 Hz	Total Flight Time	1.9797 hrs	
Swath Overlap 50% Sca		Scan Angle	± 21°	Total Laser Time	0.4156 hrs
Point Density 4.68 p/m ²		Scan Cutoff	3°	Total Swath Area	18.955 km ²
		Scan Offset	0	Total AOI Area	15.8 km ²

Table 2 – Shotgun Creek area survey totals. Area of Interest is abbreviated AOI.

Figure 3 show screen captures from the planning software displaying the planned flight lines along with other survey parameters for the Twin Creek area; these are also summarized in table 3. Finally the combined survey totals for both areas are presented in table 4.

ALTM-NAV Planner 2.1.25 - [R_Lloyd,pin] ALTM-NAV Hight Log Flight Plan GPS LIDAR Pilot Display Help		
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Scan Cutoff (deg)		
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Survey Totals		A Property Co
Total Passes 45 Swath Area (km^2) 54.844	GI LA PEL- MUTUUM	
Total Length (km) 273.864 AOI Area (km^2) 42.14		
Total Flight Time 05:01:03 Total Laser Time 01:16:04		
Costs	144 A 147	
C Use Swath Area Cost per Acre 0 Area Cost \$0 • Use ADI Area Cost per Hour 0 Time Cost \$0	A CONTRACTOR	er!
Options Errors DEM Tools Apply Help Export to KML Close		

Figure 3 Flight lines for the Twin Creek from the planning software.

Nominal Flight	Parameters	Equipment S	ettings	Area Totals	
Flight Altitude	650 m	Laser PRF	70 kHz	Total Passes	26
Flight Speed 60 m/s		Beam Divergence	0.25 mrad	Total Length	184.115 km
Swath Width 422.4 m Scan Freq		Scan Frequency	40 Hz	Total Flight Time	3.0024 hrs
Swath Overlap 50%		Scan Angle	± 21°	Total Laser Time	0.8525 hrs
Point Density 4.68 p/m ²		Scan Cutoff	3°	Total Swath Area	35.889 km ²
		Scan Offset	0	Total AOI Area	26.34 km ²

Table 3 – Shotgun Creek area survey totals. Area of Interest is abbreviated AOI.

Survey Totals						
Total Passes	45					
Total Length	273.684 km					
Total Flight Time	5.0175 hrs					
Total Laser Time	1.2678 hrs					
Total Swath Area	54.844 km ²					
Total AOI Area	42.14 km ²					

Table 4 – Both areas survey totals. Area of Interest is abbreviated AOI.

4. LiDAR and GPS Data Collection Campaign.

This survey was flown on August 31, 2009 (DOY 243) in a single flight consisting of 50 flight lines (including cross lines). The total flight time was over 4.6 hours, with a total Laser-On Time of 1.58 Hours.

Two GPS reference station locations were temporary set by NCALM during the survey; labeled MISL and LOLA. MISL was set on the grounds of the Missoula Regional Airport and LOLA was set up near the intersection of Lolo Creek Road (State Road 12) with Elk Meadows Rd. The distance between MISL and the center of the polygons of Shotgun Creek and Twin Creek are roughly 37.51 and 55 km respectively and from MISI were roughly 60.3 and 77.3 km. All reference GPS observations were logged at 1 Hz. GPS ground station equipment consisted of ASHTECH (Thales Navigation) Z-Extreme receiver, with choke ring antenna (Part# 700936.D) mounted on 1.3-meter fixed-height tripod. The airborne receiver is an integrated GPS receiver module Trimble BD950, logging at 10 Hz. Figure 4 shows the location of the stations relative to the survey polygons.



Figure 4. GPS stations and survey polygon location.

5. Data Processing and Final Product Generation.

5.1 GPS & INS Navigation Solution.

Reference coordinates for the MISL and LOLA stations were derived from a single observation session taken over the project duration and submitted to the NGS on-line processor OPUS which processes static differential baselines tied to the international CORS network. The OPUS solutions for both stations vielded reference station coordinate solutions with differences less than 0.050 meters in both horizontal and For further information **OPUS** vertical components. on see information on the CORS http://www.ngs.noaa.gov/OPUS/ and for more network see http://www.ngs.noaa.gov/CORS/. OPUS solutions for reference stations MISL and LOLA for DOY 243 are included as Appendix A & B.

Airplane trajectories for this survey were processed using KARS (Kinematic and Rapid Static) software by Dr. Gerald Mader of the NGS Research Laboratory. KARS kinematic GPS processing uses the dual-frequency phase history files of the reference and airborne receivers to determine a high-accuracy fixed integer ionosphere-free differential solution at 1 Hz. Trajectories are obtained per reference station then the trajectories are differenced with one another. The standard deviation of the difference components for trajectories processed from LOLA and MISL are 0.017, 0.022, and 0.027 meters for the East, North and Up component respectively. The final selected trajectory was derived from the KPEL station observations.

After GPS processing, the trajectory solution and the raw inertial measurement unit (IMU) data collected during the flights are combined in APPLANIX software POSPac MMS (Mobile Mapping Suite Version 5.2). POSPac MMS implements a Kalman Filter algorithm to produce a final, smoothed, and complete navigation solution including both aircraft position and orientation at 200 Hz. This final navigation solution is known as an SBET (Smoothed Best Estimated Trajectory).

5.2 Laser point processing

An SBET together with laser ranges and mirror angles are finally combined in Optech's DashMap software (Version 4.0027) to generate a flight-strip point cloud in LAS format. All point cloud coordinates were processed with respect to **NAD83** and referenced to the international CORS network. The projection is UTM Zone 11, with units in meters.

Scan angle cut-offs are done to improve the overall DEM accuracy as points farthest from the scan nadir are the most affected by small errors in pitch, roll and scanner mirror angle measurements. Moreover, scan angle cut-offs are done to eliminate points at the edge of the scan lines for improving the overall DEM accuracy as the points farthest from the scan nadir are the most affected by small errors in pitch, roll and scanner mirror angle measurements. A scan cutoff angle of 4 degrees was used.

The elevation values outputted by the DashMap software are ellipsoid heights above the NAD83 ellipsoid. These values were converted to **NAVD88 orthometric heights** computed using the **NGS GEOID 03** with the Corpscon 6 conversion software. A second set of flight-strip point cloud data files

in LAS format was generated by the elevation conversion. This dataset was used for all further processing.

5.3 Calibration

Relative calibration is done for each flight by the following method:

- 1. Planning and flying swaths with 50% side lap.
- 2. Surveying crossing flight-lines over calibration areas and over the project polygon.
- 3. Analyzing these overlaps and cross-lines in TerraMatch software. (see http://www.terrasolid.fi/en/products/4).

TerraMatch employs a least-squares approach (minimizing the height differences between computed laser surfaces from individual crossing and/or overlapping flight lines) to calculate the best-fit values for four parameters: three bore sight angle alignments (roll, pitch, and yaw), and the scanner mirror-angle scale factor.

The TerraMatch relative calibration procedure reduced the flighlines dz RMS from a starting value of 0.097 to 0.075.

Below is the TerraMatch report for the calibration site:

```
Used loaded points

Trajectories: E:\09_242_Lloyd\TerraScan\trj

No known points

Observe every 1th point

Solution for whole data set

Starting dz RMS: 0.0975

Final dz RMS: 0.0750

Standard error of unit 0.0335

Execution time: 6450.5 sec

Number of iterations: 24

Points 5971363

H shift +0.0309 Std dev 0.0003

R shift +0.0173 Std dev 0.0002

P shift +0.0098 Std dev 0.0001

Scale +0.00018
```

5.4 Classification

TerraSolid's TerraScan software was used to classify the raw laser point into the following categories: ground, non-ground (default), aerial points and low points. The processing is done by dividing each section into 1000m X 1000m tiles. For the two project areas a total of 112 tiles were created. A macro

containing the classification steps is created, which is run on each tile with a 40 m buffer. This overlap ensures consistent results for corners and edges of the tile.

Various classification algorithms which were used are given below:

1) **Isolated Points:** This routine classifies points which do not have very many other points within a 3D search radius. This routine is useful for finding isolated points up in the air (fog) or below the ground (multipath). When possibly classifying one point, this routine will find how many neighboring points there are within a given 3D search radius. It will classify the point if it does not have enough neighbors.

2) **Air points:** It classifies points which are clearly higher than the median elevation of surrounding points. It can be used to classify noise up in the air. When possibly classifying one point, this routine will find all the neighboring source points within a given search radius. It will compute the median elevation of the points and the standard deviation of the elevations. The point will be classified only if it is more than a certain limit (user defined) times the standard deviation above the median elevation. Comparison using standard deviation results in the routine being less likely to classify points in places where there is greater elevation variation.

3) Low Points: This routine was used to search for possible error points which are clearly below the ground surface. The elevation of each point (=center) is compared with every other point within a given neighborhood and if the center point is clearly lower then any other point it will be classified as a "low point". This routine can also search for groups of low points where the whole group is lower than other points in the vicinity. Input parameters used were:

4) Ground Classification: This routine classifies ground points by iteratively building a triangulated surface model. The algorithm starts by selecting some local low points assumed as sure hits on the ground, within a specified windows size. This makes the algorithm particularly sensitive to low outliers in the initial dataset, hence the requirement of removing as many erroneous low points as possible in the first step. The routine builds an initial model from selected low points. Triangles in this initial model are mostly below the ground with only the vertices touching ground. The routine then starts molding the model upwards by iteratively adding new laser points to it. Each added point makes the model follow ground surface more closely.

Ground classification parameters used:

```
Max Building Size (window size): 40.0 m
Max Terrain Angle: 88.0
Iteration Angle: 6.2
Iteration Distance: 2.0 m
```

5) Classify By Height Above Ground: It classifies points which are within a given height range compared to the ground points surface model. The routine requires that you have already classified ground points successfully. This routine will build a temporary triangulated surface model from ground points and compare other points against the elevation of the triangulated model. This routine was used to filter out the noise because of clouds hovering above the ground surface around a constant altitude.

6) Classify Below Surface: This routine classifies points which are lower than neighboring points in the source class. This routine was run after ground classification to locate points which were below the true ground surface

The use of these classification algorithms depends on the nature of topography, vegetation characteristics and extent of urbanization.

5.5 DEM production

After classification two separate sets of overlapping (40m overlap) data tiles were outputted in ASCII XYZ format: one for the ground points (filtered) and one for ground and non-ground points combined (unfiltered). The ASCII tiles were gridded using Kriging interpolation at 1m cell size resolution using Golden Software's SURFER ver. 8.01. The tile overlap is required in order to obtain a consistent surface transition from one tile to the adjacent ones when merged.

The following parameters were used for Kriging:

```
Variogram type: Linear
Nugget Variance: 0.15 m
MicroVariance: 0.00 m
SearchDataPerSector: 7
SearchMinData: 5
SearchMaxEmpty: 1
SearchRadius: 5m (unfiltered), 40m (filtered)
```

The resulted Surfer binary grids were converted to ArcInfo raster format and mosaicked together into a seamless DEM using in-house Perl and AML scripts. Two separate mosaics were produced: one for the bare-earth surface (filtered) and one for the unfiltered (default) surface.

6. Deliverables Description.

Deliverables include the following:

- 1. Point Cloud in LAS format, classified as ground or non-ground, in 1 sq. km tiles.
- 2. ESRI format 1-m DEM from ground classified points.
- 3. ESRI format 1-m DEM from all points (canopy included).
- 4. Unfiltered point cloud in ASCII format.
- 5. Filtered (bare-earth) point cloud in ASCII format.

The point cloud files are delivered in the 1000m x 1000m tiles in LAS 1.1 format. It is a binary format contains all the information associated with each point i.e. its position in X,Y,Z, intensity, flight line, timestamp, scan angle etc. The individual Las files can be converted to ASCII using the LAS to ASCII converter tool developed by the UNC. It can be accessed at <u>http://www.cs.unc.edu/~isenburg/lastools</u> It gives users the freedom to create ASCII files with whichever point features they want to access. The complete LAS 1.1 specification can be found at this address: http://liblas.org/raw-attachment/wiki/WikiStart/asprs_las_format_v11.pdf

The point classes used for this project are slightly different from the ASPRS list found in the LAS 1.1 specification. The following values can be found in the LAS Classification field:

1 - unclassified
 2 - ground
 7 - low point
 9 - aerial point
 10 - isolated point

The file naming convention for the LAS tiles is the following: bXXXXXX_YYYYYY.las , where (XXXXX, YYYYYYY) is the lower left corner tile coordinate in UTM projection.

For convenience, filtered (bare-earth) and unfiltered tiles are also provided in ASCII XYZ format. These files follow the same naming convention as the LAS tiles. Bare-earth point cloud tiles are prefixed with "f" and unfiltered point cloud tiles are prefixed with "u".

The project for all point cloud data (LAS and ASCII) is UTM zone 11N, NAVD88.

7. Appendices

APPENDIX A – OPUS Solutions for MISL GPS Reference Station

FILE: MISL243z.090 000057831

TIGED: defermencesfl edu

1008 NOTE: Antenna offsets supplied by the user were zero. Coordinates 1008 returned will be for the antenna reference point (ARP). 1008 NGS OPUS SOLUTION REPORT _____

All computed coordinate accuracies are listed as peak-to-peak values. For additional information: http://www.ngs.noaa.gov/OPUS/about.html#accuracy

USER: jcfernan@ufl.edu	DATE: February 10, 2010
RINEX FILE: misl2430.090	TIME: 17:31:05 UTC

SOFTWARE: EPHEMERIS: NAV FILE: ANT NAME: ARP HEIGHT	page5 0909.08 master igs15471.eph [precise brdc2430.09n ASH700936D_M NONE : 0.0	.pl 0810233]	START: 2009/08/31 STOP: 2009/08/31 OBS USED: 15629 / 1629 # FIXED AMB: 66 / 7 OVERALL RMS: 0.009(m)	14:51:00 20:47:00 3 : 96% 5 : 88%
REF FRAME:	NAD_83(CORS96)(EPOCH:	2002.0000)	ITRF00 (EPOCH:2	009.6650)
X: Y: Z:	-1780582.138(m) -3985592.738(m) 4636019.699(m)	0.018(m) 0.016(m) 0.015(m)	-1780582.914(m) -3985591.525(m) 4636019.703(m)	0.018(m) 0.016(m) 0.015(m)
LAT: E LON: W LON: EL HGT: ORTHO HGT:	46 54 54.02585 245 55 37.46510 114 4 22.53490 963.932(m) 978.857(m)	0.006(m) 0.010(m) 0.010(m) 0.026(m) 0.095(m) []	46 54 54.04464 245 55 37.40824 114 4 22.59176 963.394(m) NAVD88 (Computed using GEO	0.006(m) 0.010(m) 0.010(m) 0.026(m) ID09)]
	UTM COORD: UTM (Zone	INATES S' e 11)	TATE PLANE COORDINATES SPC (2500 MT)	

UTM (Zone 11)	SPC (2500 MT)
] 5199878.908	306294.338
] 722878.727	252059.188
s] 2.13863868	-3.34511486
1.00021058	0.99939408
1.00005948	0.99924310
	UTM (Zone 11) 5199878.908 722878.727 2.13863868 1.00021058 1.00005948

US NATIONAL GRID DESIGNATOR: 11TQM2287899878(NAD 83)

				BASE	STAT	IONS	USED		
PID	DI	SIGNATION	1				LATITUDE	LONGITUDE	DISTANCE(m)
DK4101	PLS5	POLSON 5	CORS AF	۲P			N473949.553	3 W1140650.07	8 83314.0
DE8232	MSOL	MISSOULA	CORS AF	۲P			N465545.83	7 W1140631.84	6 3169.8
DI2254	P046	CLEARWATE	ERMT2006	5 CORS	ARP		N470146.523	3 W1131954.18	5 57833.7
		NEARE	EST NGS	PUBLI	SHED	CONTE	ROL POINT		
RY0010		MISSOULA	BASE A	STA RI	м 1		N465448.702	2 W1140401.34	4 476.9

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

APPENDIX B – OPUS Solutions for LOLA GPS Reference Station

FILE: LOLA243z.090 000057829

1008	NOTE: Antenna offset	s supplied by the user were zero. Coordinates
1008	returned will be for	the antenna reference point (ARP).
1008		
		NGS OPUS SOLUTION REPORT

All computed coordinate accuracies are listed as peak-to-peak values. For additional information: http://www.ngs.noaa.gov/OPUS/about.html#accuracy

USER: jcfernan@ufl.edu RINEX FILE: lola243n.090			DATE: February 10, 2010 TIME: 17:30:47 UTC					
SOFTWARE: page5 0909 EPHEMERIS: igs15471.eph NAV FILE: brdc2430.09n ANT NAME: ASH700936D_N ARP HEIGHT: 0.0	.08 master5 h [precise] n M NONE	60.pl 0810	023 OBS # FIXE OVERA	START STOP USED ED AMB ALL RMS	: 2009 : 2009 : 1883 : : : : :	9/08/31 9/08/31 13 / 195 71 / 011(m)	13:5 21:3 06 81	7:00 0:30 : 96% : 88%
REF FRAME: NAD_83(CORS	96)(EPOCH:2	2002.0000)	ľ	rrf00	(EPOCH:	2009.	6650)
X: -1799914	4.309(m)	0.017(m)		-1799	9915.0	084(m)	0.01	7(m)
Y: -3990472	2.739(m)	0.012(m)		-3990	0471.	526(m)	0.01	2(m)
Z: 4624574	4.574(m)	0.006(m)		4624	4574.	578(m)	0.00	6(m)
LAT: 46 45 48.4	40125	0.011(m)	4	46 45 4	48.419	991	0.01	1(m)
E LON: 245 43 19.	58378	0.011(m)	24	15 43 3	19.52	700	0.01	1(m)
W LON: 114 16 40.4	41622	0.011(m)	11	4 16 4	40.473	300	0.01	1(m)
EL HGT: 1076	6.529(m)	0.015(m)			1075.9	993(m)	0.01	5(m)
ORTHO HGT: 1093	1.139(m)	0.093(m)	[NAVD88	(Compi	uted 1	using GE	OID09)]
	UTM COORDI	NATES	STATE PI	LANE CO	ORDII	NATES		
	UTM (Zone	e 11)	SPC	(2500	MT)		
Northing (Y) [meters]	5182475	5.654	29	0417.8	854			
Easting (X) [meters]	707856	5.618	23	35456.2	243			
Convergence [degrees]	1.9838	34798	-3.	495049	910			
Point Scale	1.0001	3106	0.	99940	204			
Combined Factor	0.9999	6232	0.	99923	342			
US NATIONAL GRID DESIGN	NATOR: 11TÇ	0M07856824	475(NAD 8	33)				
	BASE	: STATIONS	5 USED					

			51101	0111110110	0010		
PID	DI	ESIGNATION	I		LATITUDE	LONGITUDE	DISTANCE(m)
DK4103	PLS6	POLSON 6	CORS ARP		N473949.529	W1140651.393	100872.0
DE8232	MSOL	MISSOULA	CORS ARP		N465545.837	W1140631.846	22511.8
DI2254	P046	CLEARWATH	ERMT2006 CORS	ARP	N470146.523	W1131954.185	77949.2
		NEARE	EST NGS PUBLIS	SHED CONTI	ROL POINT		
RY0075		HIGHWAY 1	L2 STA 819+94		N464551.	W1141647.	161.0

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

NGS OPUS SO	LUTION REPORT		
	==========		
All computed For addition	d coordinate accuracies are list nal information: www.ngs.noaa.go	ted as peak-to-peak values. ov/OPUS/Using_OPUS.html#acc	uracy
USER: RINEX FILE:	michaels@ufl.edu 5sis118m.09o	DATE: May 05, 200 TIME: 18:30:17 UT	9
SOFTWARE: EPHEMERIS: NAV FILE: ANT NAME: ARP HEIGHT:	page5 0810.20 master12.pl 0810 igr15292.eph [rapid] brdc1180.09n ASH700936D_M NONE 1.300	023 START: 2009/04/28 STOP: 2009/04/28 OBS USED: 25524 / 260 # FIXED AME: 94 / 1 OVERALL RMS: 0.018(m)	12:53:00 22:48:30 64 : 98% 06 : 89%
REF FRAME:	NAD_83(CORS96)(EPOCH:2002.0000) ITRF00 (EPOCH:	2009.3225)
X: Y: Z:	111002.407(m)0.012(m)-6099384.360(m)0.034(m)1856993.382(m)0.022(m)	111001.736(m) -6099382.692(m) 1856993.106(m)	0.012(m) 0.034(m) 0.022(m)
LAT: E LON: W LON: EL HGT: ORTHO HGT:	17 2 16.95295 0.027(m) 271 2 33.38910 0.012(m) 88 57 26.61090 0.012(m) 458.025(m) 0.029(m) [No NGS Geoid Model Available	17 2 16.96038 271 2 33.36744 88 57 26.63256 456.338(m) (FAQ 21).]	0.027(m) 0.012(m) 0.012(m) 0.029(m)
Northing (Y Easting (X) Convergence	UTM COORDINATES UTM (Zone 16))[meters] 1884806.536 [meters] 291657.153 :[degrees] -0.57373658	STATE PLANE COORDINATES *** NOTE *** Please manually select SPC zone.	

		OIN COORDINATED	DIATE I DAME COORDINATED
		UTM (Zone 16)	*** NOTE ***
Northing (Y)	[meters]	1884806.536	Please manually select
Easting (X)	[meters]	291657.153	SPC zone.
Convergence	[degrees]	-0.57373658	
Point Scale		1.00013675	
Combined Facto	or	0.0000000	

US NATIONAL GRID DESIGNATOR: 16QBD9165784807(NAD 83)

	BASE STAT	IONS USED		
PID	DESIGNATION	LATITUDE	LONGITUDE	DISTANCE(m)
AI7441	GUAT GUATEMALA CITY CORS ARP	N143525.448	W0903112.637	318427.6
AI8353	SSIA SAN SALVADOR CORS ARP	N134149.499	W0890659.724	370059.6
DH8188	CHET CHETUMAL CORS ARP			175737.7
	NEAREST NGS PUBLISHED	CONTROL POINT		
AJ8058	SANTA ELENA CORS ARP	N165457.793	W0895203.387	97855.9

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.