# EFFECTS OF WATERSHED RESTORATION ON HILLSLOPE STABILITY AND ECOHYDROLOGICAL FUNCTIONS 

Mapping Project Report

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## 1. LiDAR System Description and Specifications

This survey was performed with an Optech GEMINI Airborne Laser Terrain Mapper (ALTM) serial number 06SEN195 mounted in a twin-engine Cessna Skymaster (Tail Number N337P). The instrument specifications are listed in table 1.

| Operating Altitude | $150-4000 \mathrm{~m}$, Nominal |
| :--- | :--- |
| Horizontal Accuracy | $1 / 5,500 \times$ altitude $(\mathrm{m}$ AGL); 1 sigma |
| Elevation Accuracy | $5-30 \mathrm{~cm} ; 1$ sigma |
| Range Capture | Up to 4 range measurements, including $1^{\text {st }}, 2^{\text {nd }}, 3^{\text {rd }}$, last returns |
| Intensity Capture | 12 -bit dynamic range for all recorded returns, including last returns |
| Scan FOV | $0-50$ degrees; Programmable in increments of $\pm 1$ degree |
| Scan Frequency | $0-70 \mathrm{~Hz}$ |
| Scanner Product | Up to Scan angle $\times$ Scan frequency $=1000$ |
| Roll Compensation | $\pm 5$ degrees at full FOV - more under reduced FOV |
| Pulse Rate Frequency | $33-167 \mathrm{kHz}$ |
| Position Orientation System | Applanix POS/AV 510 OEM includes embedded BD950 12- |


|  | channel 10 Hz GPS receiver |
| :--- | :--- |
| Laser Wavelength/Class | 1047 nanometers / Class IV (FDA 21 CFR) |
| Beam Divergence nominal ( full angle) | Dual Divergence $0.25 \mathrm{mrad}(1 / \mathrm{e})$ or $0.80 \mathrm{mrad}(1 / \mathrm{e})$ |

Table 1 - Optech GEMINI specifications.
See http://www.optech.ca for more information from the manufacturer. http://www.optech.ca/pdf/Brochures/ALTM-GEMINI.pdf

## 2. Description of Pl's Areas of Interest.

The areas of interest are two experimental watersheds, Shotgun Creek and Twin Creek located in the Clearwater National Forest of northern Idaho. These areas are roughly 70 km southwest of Missoula, MT. and are delimited by two irregular polygons as shown in figure 1 (Google Maps image). The survey polygon for Shotgun Creek (Area 1) is approximately 15.8 square kilometers and for Twin Creek (Area 2) is 26.34 square kilometers. The polygon for area 1 is roughly 5 km long in the EastWest orientation and 3.5 km long in the North-South direction. Area 2 has a maximum length of 8.86 km in the $155^{\circ}$ azimuth with an average width of 2.77 km .


Figure 1 - Shape and location of survey polygon (Google Maps).

## 3. Airborne Survey Planning Process.

The survey planning was performed considering nominal values of 650 m for flight altitude above the terrain, a mean flying speed of $60 \mathrm{~m} / \mathrm{s}$ and a swath overlap of $50 \%$. Taken into account these values and the layout of the areas of interest the optimized flight plan consisted of a total of 45 flight lines, 19 for Shotgun creek at azimuths of $90 / 270^{\circ}$ and 26 for Twin creek at azimuths of $155 / 335^{\circ}$. In order to obtain the highest point density the laser Pulse Repetition Frequency (PRF) was set to 70 kHz . Scan frequency (mirror oscillation rate) was held to 40 Hz and the scan angle (Field-of-View or FOV) was limited to +/- 21 degrees. These parameters yield a scan product (frequency $x$ angle) of 840 out of a system maximum of 1000 , or about $84 \%$ of system limits. The combination of all these parameters should yield a point density of 4.7 points per $\mathrm{m}^{2}$. Figure 2 show screen captures from the planning software displaying the planned flight lines along with other survey parameters for the Shotgun Creek area; these are also summarized in table 2.


Figure 2. East-West flight lines for Shotgun Creek from the planning software.

| Nominal Flight Parameters |  | Equipment Settings |  | Area Totals |  |
| :--- | :---: | :--- | :---: | :--- | :---: |
| Flight Altitude | 650 m | Laser PRF | 70 kHz | Total Passes | 19 |
| Flight Speed | $60 \mathrm{~m} / \mathrm{s}$ | Beam Divergence | 0.25 mrad | Total Length | 89.749 km |
| Swath Width | 422.4 m | Scan Frequency | 40 Hz | Total Flight Time | 1.9797 hrs |
| Swath Overlap | $50 \%$ | Scan Angle | $\pm 21^{\circ}$ | Total Laser Time | 0.4156 hrs |
| Point Density | $4.68 \mathrm{p} / \mathrm{m}^{2}$ | Scan Cutoff | $3^{\circ}$ | Total Swath Area | $18.955 \mathrm{~km}^{2}$ |

Table 2 - Shotgun Creek area survey totals. Area of Interest is abbreviated AOI.

Figure 3 show screen captures from the planning software displaying the planned flight lines along with other survey parameters for the Twin Creek area; these are also summarized in table 3. Finally the combined survey totals for both areas are presented in table 4.


Figure 3 Flight lines for the Twin Creek from the planning software.

| Nominal Flight Parameters |  | Equipment Settings |  | Area Totals |  |
| :--- | :---: | :--- | :---: | :--- | :---: |
| Flight Altitude | 650 m | Laser PRF | 70 kHz | Total Passes | 26 |
| Flight Speed | $60 \mathrm{~m} / \mathrm{s}$ | Beam Divergence | 0.25 mrad | Total Length | 184.115 km |
| Swath Width | 422.4 m | Scan Frequency | 40 Hz | Total Flight Time | 3.0024 hrs |
| Swath Overlap | $50 \%$ | Scan Angle | $\pm 21^{\circ}$ | Total Laser Time | 0.8525 hrs |
| Point Density | $4.68 \mathrm{p} / \mathrm{m}^{2}$ | Scan Cutoff | $3^{\circ}$ | Total Swath Area | $35.889 \mathrm{~km}^{2}$ |
|  |  | Scan Offset | 0 | Total AOI Area | $26.34 \mathrm{~km}^{2}$ |

Table 3 - Shotgun Creek area survey totals. Area of Interest is abbreviated AOI.

| Survey Totals |  |
| :---: | :---: |
| Total Passes | 45 |
| Total Length | 273.684 km |
| Total Flight Time | 5.0175 hrs |
| Total Laser Time | 1.2678 hrs |
| Total Swath Area | $54.844 \mathrm{~km}^{2}$ |
| Total AOI Area | $42.14 \mathrm{~km}^{2}$ |

Table 4 - Both areas survey totals. Area of Interest is abbreviated AOI.

## 4. LiDAR and GPS Data Collection Campaign.

This survey was flown on August 31, 2009 (DOY 243) in a single flight consisting of 50 flight lines (including cross lines). The total flight time was over 4.6 hours, with a total Laser-On Time of 1.58 Hours.

Two GPS reference station locations were temporary set by NCALM during the survey; labeled MISL and LOLA. MISL was set on the grounds of the Missoula Regional Airport and LOLA was set up near the intersection of Lolo Creek Road (State Road 12) with Elk Meadows Rd. The distance between MISL and the center of the polygons of Shotgun Creek and Twin Creek are roughly 37.51 and 55 km respectively and from MISI were roughly 60.3 and 77.3 km . All reference GPS observations were logged at 1 Hz . GPS ground station equipment consisted of ASHTECH (Thales Navigation) ZExtreme receiver, with choke ring antenna (Part\# 700936.D) mounted on 1.3-meter fixed-height tripod. The airborne receiver is an integrated GPS receiver module Trimble BD950, logging at 10 Hz . Figure 4 shows the location of the stations relative to the survey polygons.


Figure 4. GPS stations and survey polygon location.

## 5. Data Processing and Final Product Generation.

### 5.1 GPS \& INS Navigation Solution.

Reference coordinates for the MISL and LOLA stations were derived from a single observation session taken over the project duration and submitted to the NGS on-line processor OPUS which processes static differential baselines tied to the international CORS network. The OPUS solutions for both stations yielded reference station coordinate solutions with differences less than 0.050 meters in both horizontal and vertical components. For further information on OPUS see http://www.ngs.noaa.gov/OPUS/ and for more information on the CORS network see http://www.ngs.noaa.gov/CORS/ . OPUS solutions for reference stations MISL and LOLA for DOY 243 are included as Appendix A \& B.

Airplane trajectories for this survey were processed using KARS (Kinematic and Rapid Static) software by Dr. Gerald Mader of the NGS Research Laboratory. KARS kinematic GPS processing uses the dual-frequency phase history files of the reference and airborne receivers to determine a highaccuracy fixed integer ionosphere-free differential solution at 1 Hz . Trajectories are obtained per reference station then the trajectories are differenced with one another. The standard deviation of the difference components for trajectories processed from LOLA and MISL are 0.017, 0.022, and 0.027 meters for the East, North and Up component respectively. The final selected trajectory was derived from the KPEL station observations.

After GPS processing, the trajectory solution and the raw inertial measurement unit (IMU) data collected during the flights are combined in APPLANIX software POSPac MMS (Mobile Mapping Suite Version 5.2). POSPac MMS implements a Kalman Filter algorithm to produce a final, smoothed, and complete navigation solution including both aircraft position and orientation at 200 Hz . This final navigation solution is known as an SBET (Smoothed Best Estimated Trajectory).

### 5.2 Laser point processing

An SBET together with laser ranges and mirror angles are finally combined in Optech's DashMap software (Version 4.0027) to generate a flight-strip point cloud in LAS format. All point cloud coordinates were processed with respect to NAD83 and referenced to the international CORS network. The projection is UTM Zone 11, with units in meters.

Scan angle cut-offs are done to improve the overall DEM accuracy as points farthest from the scan nadir are the most affected by small errors in pitch, roll and scanner mirror angle measurements. Moreover, scan angle cut-offs are done to eliminate points at the edge of the scan lines for improving the overall DEM accuracy as the points farthest from the scan nadir are the most affected by small errors in pitch, roll and scanner mirror angle measurements. A scan cutoff angle of 4 degrees was used.

The elevation values outputted by the DashMap software are ellipsoid heights above the NAD83 ellipsoid. These values were converted to NAVD88 orthometric heights computed using the NGS GEOID 03 with the Corpscon 6 conversion software. A second set of flight-strip point cloud data files
in LAS format was generated by the elevation conversion. This dataset was used for all further processing.

### 5.3 Calibration

Relative calibration is done for each flight by the following method:

1. Planning and flying swaths with $50 \%$ side lap.
2. Surveying crossing flight-lines over calibration areas and over the project polygon.
3. Analyzing these overlaps and cross-lines in TerraMatch software. (see http://www.terrasolid.fi/en/products/4).

TerraMatch employs a least-squares approach (minimizing the height differences between computed laser surfaces from individual crossing and/or overlapping flight lines) to calculate the best-fit values for four parameters: three bore sight angle alignments (roll, pitch, and yaw), and the scanner mirrorangle scale factor.

The TerraMatch relative calibration procedure reduced the flighlines dz RMS from a starting value of 0.097 to 0.075 .

Below is the TerraMatch report for the calibration site:

```
Used loaded points
Trajectories: E:\09_242_Lloyd\TerraScan\trj
No known points
Observe every 1th point
Solution for whole data set
Starting dz RMS: 0.0975
Final dz RMS: 0.0750
Standard error of unit 0.0335
Execution time: 6450.5 sec
Number of iterations: 24
Points }597136
H shift +0.0309 Std dev 0.0003
R shift +0.0173 Std dev 0.0002
P shift +0.0098 Std dev 0.0001
Scale +0.00018
```


### 5.4 Classification

TerraSolid's TerraScan software was used to classify the raw laser point into the following categories: ground, non-ground (default), aerial points and low points. The processing is done by dividing each section into 1000 m X 1000 m tiles. For the two project areas a total of 112 tiles were created. A macro
containing the classification steps is created, which is run on each tile with a 40 m buffer. This overlap ensures consistent results for corners and edges of the tile.

Various classification algorithms which were used are given below:

1) Isolated Points: This routine classifies points which do not have very many other points within a 3D search radius. This routine is useful for finding isolated points up in the air (fog) or below the ground (multipath). When possibly classifying one point, this routine will find how many neighboring points there are within a given 3D search radius. It will classify the point if it does not have enough neighbors.
2) Air points: It classifies points which are clearly higher than the median elevation of surrounding points. It can be used to classify noise up in the air. When possibly classifying one point, this routine will find all the neighboring source points within a given search radius. It will compute the median elevation of the points and the standard deviation of the elevations. The point will be classified only if it is more than a certain limit (user defined) times the standard deviation above the median elevation. Comparison using standard deviation results in the routine being less likely to classify points in places where there is greater elevation variation.
3) Low Points: This routine was used to search for possible error points which are clearly below the ground surface. The elevation of each point (=center) is compared with every other point within a given neighborhood and if the center point is clearly lower then any other point it will be classified as a "low point". This routine can also search for groups of low points where the whole group is lower than other points in the vicinity. Input parameters used were:
4) Ground Classification: This routine classifies ground points by iteratively building a triangulated surface model. The algorithm starts by selecting some local low points assumed as sure hits on the ground, within a specified windows size. This makes the algorithm particularly sensitive to low outliers in the initial dataset, hence the requirement of removing as many erroneous low points as possible in the first step. The routine builds an initial model from selected low points. Triangles in this initial model are mostly below the ground with only the vertices touching ground. The routine then starts molding the model upwards by iteratively adding new laser points to it. Each added point makes the model follow ground surface more closely.

Ground classification parameters used:

```
Max Building Size (window size): 40.0 m
Max Terrain Angle: 88.0
Iteration Angle: 6.2
Iteration Distance: 2.0 m
```

5) Classify By Height Above Ground: It classifies points which are within a given height range compared to the ground points surface model. The routine requires that you have already classified ground points successfully. This routine will build a temporary triangulated surface model from ground points and compare other points against the elevation of the triangulated model. This routine was used to filter out the noise because of clouds hovering above the ground surface around a constant altitude.
6) Classify Below Surface: This routine classifies points which are lower than neighboring points in the source class. This routine was run after ground classification to locate points which were below the true ground surface

The use of these classification algorithms depends on the nature of topography, vegetation characteristics and extent of urbanization.

### 5.5 DEM production

After classification two separate sets of overlapping (40m overlap) data tiles were outputted in ASCII XYZ format: one for the ground points (filtered) and one for ground and non-ground points combined (unfiltered). The ASCII tiles were gridded using Kriging interpolation at 1 m cell size resolution using Golden Software's SURFER ver. 8.01. The tile overlap is required in order to obtain a consistent surface transition from one tile to the adjacent ones when merged.

The following parameters were used for Kriging:

```
Variogram type: Linear
Nugget Variance: 0.15 m
MicroVariance: 0.00 m
SearchDataPerSector: 7
SearchMinData: 5
SearchMaxEmpty: 1
SearchRadius: 5m (unfiltered), 40m (filtered)
```

The resulted Surfer binary grids were converted to ArcInfo raster format and mosaicked together into a seamless DEM using in-house Perl and AML scripts. Two separate mosaics were produced: one for the bare-earth surface (filtered) and one for the unfiltered (default) surface.

## 6. Deliverables Description.

Deliverables include the following:

1. Point Cloud in LAS format, classified as ground or non-ground, in 1 sq . km tiles.
2. ESRI format 1-m DEM from ground classified points.
3. ESRI format 1-m DEM from all points (canopy included).
4. Unfiltered point cloud in ASCII format.
5. Filtered (bare-earth) point cloud in ASCII format.

The point cloud files are delivered in the $1000 \mathrm{~m} \times 1000 \mathrm{~m}$ tiles in LAS 1.1 format. It is a binary format contains all the information associated with each point i.e. its position in X,Y,Z, intensity, flight line, timestamp, scan angle etc. The individual Las files can be converted to ASCII using the LAS to ASCII converter tool developed by the UNC. It can be accessed at http://www.cs.unc.edu/~isenburg/lastools It gives users the freedom to create ASCII files with whichever point features they want to access. The complete LAS 1.1 specification can be found at this address: http://liblas.org/raw-attachment/wiki/WikiStart/asprs_las_format_v11.pdf

The point classes used for this project are slightly different from the ASPRS list found in the LAS 1.1 specification. The following values can be found in the LAS Classification field:

1 - unclassified
2 - ground
7 - low point
9 - aerial point
10 - isolated point
The file naming convention for the LAS tiles is the following: bXXXXXX_YYYYYYY.las , where (XXXXX, YYYYYYY) is the lower left corner tile coordinate in UTM projection.

For convenience, filtered (bare-earth) and unfiltered tiles are also provided in ASCII XYZ format. These files follow the same naming convention as the LAS tiles. Bare-earth point cloud tiles are prefixed with " f " and unfiltered point cloud tiles are prefixed with " u ".

The project for all point cloud data (LAS and ASCII) is UTM zone 11N, NAVD88.

## 7. Appendices

## APPENDIX A - OPUS Solutions for MISL GPS Reference Station

FILE: MISL243z.090 000057831
1008 NOTE: Antenna offsets supplied by the user were zero. Coordinates
1008 returned will be for the antenna reference point (ARP).
1008
NGS OPUS SOLUTION REPORT

All computed coordinate accuracies are listed as peak-to-peak values.
For additional information: http://www.ngs.noaa.gov/OPUS/about.html\#accuracy

USER: jcfernan@ufl.edu
RINEX FILE: misl243o.09o

DATE: February 10, 2010
TIME: 17:31:05 UTC

```
SOFTWARE: page5 0909.08 master.pl 0810233
EPHEMERIS: igs15471.eph [precise]
NAV FILE: brdc2430.09n
ANT NAME: ASH700936D_M NONE
ARP HEIGHT: 0.0
REF FRAME: NAD_83(CORS 96)(EPOCH:2002.0000)
```

| START: | $2009 / 08 / 31 \quad 14: 51: 00$ |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
| STOP: | $2009 / 08 / 31 \quad 20: 47: 00$ |  |  |  |
| OBS USED | $15629 / 16293:$ | $96 \%$ |  |  |
| \# FIXED AMB | $66 /$ | 75 | $:$ | $88 \%$ |
| OVERALL RMS $:$ | $0.009(\mathrm{~m})$ |  |  |  |

ITRF00 (EPOCH:2009.6650)

|  | X : | -1780582.138(m) |  |  | 0.018 (m) |  | -17 | 80582.914 (m) | 0.018 (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Y: | -3985592.738(m) |  |  | 0.016 (m) |  | -39 | 85591.525 (m) | 0.016 (m) |
|  | Z: | 4636019.699 (m) |  |  | 0.015 (m) |  |  | 36019.703 (m) | 0.015 (m) |
|  | LAT: | 46 | 54 | 54.02585 | 0.006 (m) | 46 | 54 | 54.04464 | 0.006 (m) |
| E | LON: | 245 | 55 | 37.46510 | 0.010 (m) | 245 | 55 | 37.40824 | 0.010 (m) |
| W | LON: | 114 | 4 | 22.53490 | 0.010 (m) | 114 | 4 | 22.59176 | 0.010 (m) |
| EL | HGT: |  |  | 963.932 (m) | 0.026 (m) |  |  | 963.394 (m) | 0.026 (m) |
| ORTHO | HGT: |  |  | 978.857 (m) | 0.095 (m) | [NAVD88 | Com | puted using | ID09) ] |



This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

## APPENDIX B - OPUS Solutions for LOLA GPS Reference Station

FILE: LOLA243z.090 000057829

```
1008 NOTE: Antenna offsets supplied by the user were zero. Coordinates
1008 returned will be for the antenna reference point (ARP).
```

1008
NGS OPUS SOLUTION REPORT

All computed coordinate accuracies are listed as peak-to-peak values. For additional information: http://www.ngs.noaa.gov/OPUS/about.html\#accuracy

USER: jcfernan@ufl.edu
RINEX FILE: lola243n.090

```
        DATE: February 10, }201
        TIME: 17:30:47 UTC
```

| SOFTWARE: page5 0909. | ster50.pl | 081023 | START: 2009/08/31 |  |  | 13:57:00 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EPHEMERIS: igs15471.eph | cise] |  | STOP: | 2009/08 | 08/31 |  | 30 |  |
| NAV FILE: brdc2430.09n |  |  | OBS USED: | 18813 | / 195 | 06 |  | 96\% |
| ANT NAME: ASH700936D_M | NONE |  | \# FIXED AMB: |  |  | 81 |  | 88\% |
| ARP HEIGHT: 0.0 |  |  | OVERALL RMS | 0.01 | 1 (m) |  |  |  |

REF FRAME: NAD_83 (CORS96) (EPOCH:2002.0000) ITRFOO (EPOCH:2009.6650)

|  | X : |  | -179 | 99914.309 (m) | 0.017 (m) |  | -1799915.084 (m) | 0.017 (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Y: |  | -399 | 90472.739 (m) | 0.012 (m) |  | -3990471.526 (m) | 0.012 (m) |
|  | Z: |  |  | 24574.574 (m) | 0.006 (m) |  | 4624574.578 (m) | 0.006 (m) |
|  | LAT: | 46 | 45 | 48.40125 | 0.011 (m) | 46 | 4548.41991 | 0.011 (m) |
| E | LON: | 245 | 43 | 19.58378 | 0.011 (m) | 245 | 4319.52700 | 0.011 (m) |
| W | LON: | 114 | 16 | 40.41622 | 0.011 (m) | 114 | 1640.47300 | 0.011 (m) |
| EL | HGT: |  |  | 1076.529 (m) | 0.015 (m) |  | 1075.993 (m) | 0.015 (m) |
| ORTHO | HGT : |  |  | 1091.139 (m) | 0.093 (m) | [NAVD88 | Computed using | OID09)] |

$\left.\begin{array}{llcrl} & & \text { UTM COORDINATES } & \text { STATE PLANE COORDINATES } \\ & \text { UTM (Zone 11) } & \text { SPC (2500 MT }\end{array}\right)$

US NATIONAL GRID DESIGNATOR: 11TQMO785682475 (NAD 83)


[^0]NGS OPUS SOLUTION REPORT

All computed coordinate accuracies are listed as peak-to-peak values.
For additional information: www.ngs.noaa.gov/OPUS/Using_OPUS.html\#accuracy


REF FRAME: NAD_83(CORS 96) (EPOCH:2002.0000)
ITRF00 (EPOCH:2009.3225)


| UTM COORDINATES | STATE PLANE COORDINATES |
| :---: | :---: |
| UTM (Zone 16) | $\star * *$ NOTE $* * *$ |
| 1884806.536 | Please manually select |
| 291657.153 | SPC zone. |
| -0.57373658 |  |
| 1.00013675 |  |
| 0.00000000 |  |
| ATOR: $160 \operatorname{CD} 9165784807($ NAD 83) |  |

BASE STATIONS USED

| PID | DESIGNATION | LATITUDE | LONGITUDE | DISTANCE (m) |
| :---: | :---: | :---: | :---: | :---: |
| AI7441 | GUAT GUATEMALA CITY CORS ARP | N143525.448 | W0903112.637 | 318427.6 |
| AI8353 | SSIA SAN SALVADOR CORS ARP | N134149.499 | W0890659.724 | 370059.6 |
| DH8188 | CHET CHETUMAL CORS ARP |  |  | 175737.7 |
|  | NEAREST NGS PUBLISHED | ROL POINT |  |  |
| AJ8058 | SANTA ELENA CORS ARP | N165457.793 | W0895203.387 | 97855.9 |

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.


[^0]:    This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

